

# Dependable Contact Related Parameter Extraction in Graphene–Metal Junctions

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The accurate extraction and the reliable, repeatable reduction of graphene–metal contact resistance ( $R_C$ ) are still open issues in graphene technology. Here, the importance of following clear protocols when extracting  $R_C$  using the transfer length method (TLM) is demonstrated. The example of back-gated graphene TLM structures with nickel contacts, a complementary metal oxide semiconductor compatible metal, is used here. The accurate extraction of  $R_C$  is significantly affected by generally observable Dirac voltage shifts with increasing channel lengths in ambient conditions.  $R_C$  is generally a function of the carrier density in graphene. Hence, the position of the Fermi level and the gate voltage impact the extraction of  $R_C$ . Measurements in high vacuum, on the other hand, result in dependable extraction of  $R_C$  as a function of gate voltage owing to minimal spread in Dirac voltages. The accurate measurement and extraction of important parameters like contact-end resistance, transfer length, sheet resistance of graphene under the metal contact, and specific contact resistivity as a function of the back-gate voltage is further assessed. The presented methodology has also been applied to devices with gold and copper contacts, with similar conclusions.

## 1. Introduction

Graphene exhibits unique and remarkable physical, chemical, and electrical properties.<sup>[1]</sup> It is considered as a promising material for electronic devices and applications. The extraordinary features of graphene have been explored in numerous device demonstrations such as radio frequency analog transistors,<sup>[2–7]</sup> photodetectors,<sup>[8–12]</sup> nanoelectromechanical systems,<sup>[13–17]</sup> and terahertz modulators.<sup>[18–20]</sup> Low resistivity electrical contacts are fundamental for all of these applications as they provide means for communication between the active devices and the outside world.<sup>[21]</sup> Because of the low density of states in graphene,<sup>[22]</sup> the charge injection into graphene leads to a high contact resistance ( $R_C$ ) at graphene–metal (G–M) junctions,<sup>[23]</sup> that may be a serious limiting factor for graphene devices. To achieve low contact resistivity, nanostructuring or engineering of graphene under

the contact metals have displayed some potential.<sup>[24–26]</sup> Nevertheless, reported values of  $R_C$  found in literature vary considerably,<sup>[27–30]</sup> which can be attributed to intrinsic factors such as the quality of graphene layers, work functions of the metals or doping of graphene, and to extrinsic factors such as specific fabrication procedures. However, there is also a debate on the applicability of standard measurement and extraction methods to obtain dependable and correct  $R_C$  values. In particular, the transfer length method (TLM) is widely used to extract  $R_C$  from test structures. It has been suggested and demonstrated that the classic TLM may be inappropriate under certain conditions for characterizing G–M contacts.<sup>[31–35]</sup> Since the sheet resistance of the graphene channel ( $R_{SH}$ ) is a dominating component of the total resistance of the device ( $R_T$ ), and since the TLM technique is based on the comparison of the  $R_T$  values of the graphene field effect transistors (GFETs) inside the TLM structure, slight changes in  $R_{SH}$  along the TLM array will lead to erroneous  $R_C$  values. In addition, the  $R_{SH}$  is different from the sheet resistance of graphene under the metal contact ( $R_{SK}$ ) due to the G–M interactions that dope graphene,<sup>[27,36,37]</sup> and this should be accounted for in the extraction of the parameters describing the G–M junction.


Here, we present a comprehensive analysis of the TLM technique for extracting  $R_C$  in 2D graphene devices using nickel (Ni) as contact metal. The analysis is further implemented and verified using copper (Cu) and gold (Au) contacts as well for

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generalization. In the following, we use an extended terminology, where the extracted  $R_C$  is called contact front resistance ( $R_{CF}$ ).  $R_{CF}$  is extracted from a measured voltage drop at the source/drain contacts that depends on the contact shape and size (i.e., geometry dependent), the charge carrier density ( $n_0$ ) in graphene under the metal contact, and the specific contact resistivity  $\rho_c$ , which is geometrically independent. These additional parameters can be obtained by measuring the contact-end resistance ( $R_{CE}$ ),<sup>[38]</sup> which allows extracting  $\rho_c$ , the  $R_{SK}$  and the transfer length ( $L_{TK}$ ). Furthermore,  $R_{SK}$  can be compared to  $R_{SH}$  to gain insight into the impact of the contact metal proximity to the graphene on the graphene charge. Finally, the developed method enables the identification of extrinsic effects which significantly affect the extraction of  $R_{CF}$  by comparing measurements performed in ambient and vacuum conditions ( $\approx 10^{-6}$  mbar). In particular, the shift of the Dirac voltage ( $V_{DIRAC}$ ) in devices with different channel length ( $L_{CH}$ ) influences the variability of the extracted data.

## 2. Theory

In the TLM measurement technique,  $R_{CF}$  is extracted from the total measured resistance ( $R_T$ ) of the device, which comprises of the  $R_{SH}$ , two times  $R_{CF}$  and the parasitic resistances (which are generally neglected) of the metal contact pad, probe needles, and leads. Here,  $R_T$  of a GFET is extracted by applying a voltage  $V_{12}$  between contacts 1 and 2 and measuring the current  $I_{12}$  as shown in **Figure 1a**. Therefore,

$$R_T = \frac{V_{12}}{I_{12}} \quad (1)$$

As mentioned above, the  $R_T$  of the device can be deconvoluted into

$$R_T = 2R_{CF} + \frac{R_{SH} * L_{CH}}{W_{CH}} + 2R_M \quad (2)$$

where  $R_M$  is the resistance of the metal that is generally neglected ( $R_M \ll R_{SH}$ ).  $R_{CF}$  and  $R_{SH}$  are extracted by the TLM extrapolation technique. More details about the TLM extraction technique are reported in the Section B, Supporting Information. **Figure 1b** explicitly explains about various resistive components at G–M junction. In **Figure 1b**, for the contact 2,  $X = 0$  corresponds to the front edge of the contact, while  $X = d$  is at the end of the contact (where  $d = 4 \mu\text{m}$  is the length of the fabricated contact).  $R_{CF}$  is defined as the ratio of the voltage drop across the interfacial layer at the front edge of the contact, where the current density is greatest ( $X = 0$ ) as shown in **Figure 1b**.  $R_{CE}$  instead is defined through the voltage drop across the interfacial layer at the edge of the contact, where the current density is least ( $X = d$ ) as depicted in **Figure 1b**.

As metal can dope graphene at the contact regions,<sup>[39]</sup>  $R_{SK}$  may be different from the  $R_{SH}$ .<sup>[27]</sup> If  $R_{SK} \neq R_{SH}$ , the extraction of  $L_{TK}$ , described in detail in the Section C, Supporting Information, by using the conventional extraction through the TLM method leads to erroneous  $L_{TK}$  values. In such a situation, additional measurements are required to extract reliable contact related parameters at the G–M junction, namely the  $R_{CE}$  technique.<sup>[33,38]</sup>  $R_{CE}$  can be

measured directly by forcing a known current between contacts 1 and 2 and measuring the generated voltage drop across the G–M stack, while imposing a null current on contact 3 as shown in **Figure 1a**. In this way,  $R_{CE}$  is measured by the use of the additional contact 3, since by forcing a null current, there is no additional voltage drop between contacts 2 and 3. So we have:

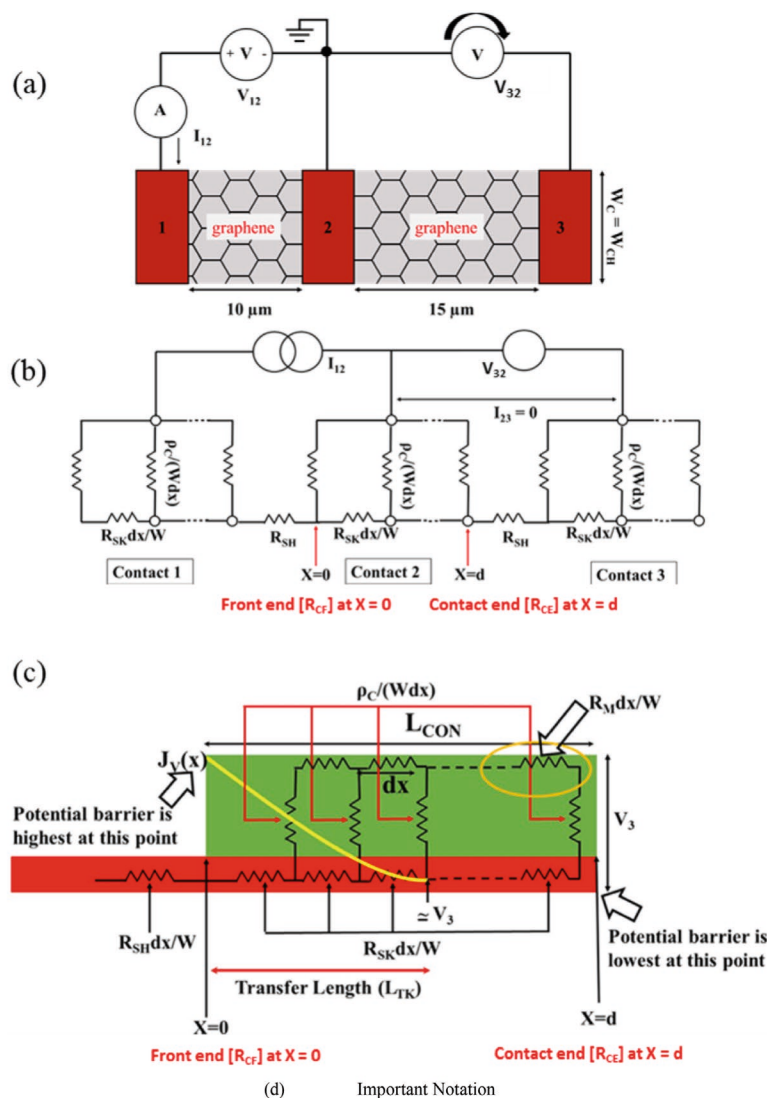
$$R_{CE} = \frac{V_{32}}{I_{12}} \quad (3)$$

The  $R_{CE}$  measurement does not depend on the graphene quality outside the metal, which removes errors caused by inhomogeneities of the graphene channel.

**Figure 1c** is the distributed resistance network describing the transmission line model typically used to describe the G–M contacts. Here, the current is highest at front edge of the contact ( $X = 0$ ) and drops exponentially with the distance (represented by a yellow line as  $Jv(x)$ ). The “ $1/e$ ” distance of the voltage drop profile from the front edge of the contact is defined as  $L_{TK}$ . In layman terms,  $L_{TK}$  is the effective electrical length of the contact. The transmission line model equations<sup>[38]</sup> can be used to extract  $\rho_c$ ,  $R_{SK}$ , and  $L_{TK}$  by using the  $R_{CF}$  and  $R_{CE}$  values measured with the procedure explained above. Further details on this point are provided in Section C, Supporting Information.

## 3. Results and Discussion

Large-area monolayer graphene was grown on a copper (Cu) foil via chemical vapor deposition (CVD) process in a NanoCVD (Moorfield, UK) rapid thermal processing tool.<sup>[40]</sup> Silicon wafers (p-doped) with resistivity ( $1\text{--}20 \Omega\mu\text{m}$ ) were used as a starting substrate and thermally oxidized to achieve a thickness of 85 nm. CVD graphene was transferred onto the silicon/silicon dioxide (Si/SiO<sub>2</sub>) substrate using an electrochemical delamination technique.<sup>[41]</sup> Photolithography and reactive ion etching were used to define graphene channels using an oxygen plasma process. Nickel (Ni), Copper (Cu), and gold (Au) metals were thermally evaporated to contact graphene, and a lift-off process was carried out in order to define source-drain contact pads. Subsequently, rapid thermal annealing process was carried out for 2 h in an argon (95%)/hydrogen (5%) atmosphere at 450 °C to minimize the PMMA residue and to enhance the G–M contact bonding.<sup>[42]</sup> **Figure 2a** shows a scanning electron micrograph of a complete TLM structure with a channel width of  $W_{CH} = 20 \mu\text{m}$  and  $L_{CH}$  ranging from 5 to 50  $\mu\text{m}$ . **Figure 2b** shows a Raman area map of the 2D band intensity in one of the TLM channels, indicated by the blue square in the optical micrograph. A mostly uniform intensity distribution was observed which pointed toward homogenous graphene layers. **Figure 2c** shows the Raman spectrum of the graphene taken before and after the final device fabrication on SiO<sub>2</sub>/Si substrate. The red curve is the Raman spectrum of graphene just after the transfer with a ratio of  $I_{2D}/I_G$  close to 2, confirming the high quality of the monolayer graphene. The potential presence of some graphene adlayers and grain boundaries result in a small D peak. The TLM structures were vacuum annealed after final device fabrication to enhance the G–M bonding.<sup>[42]</sup> The black curve in **Figure 2c** shows the Raman spectrum of

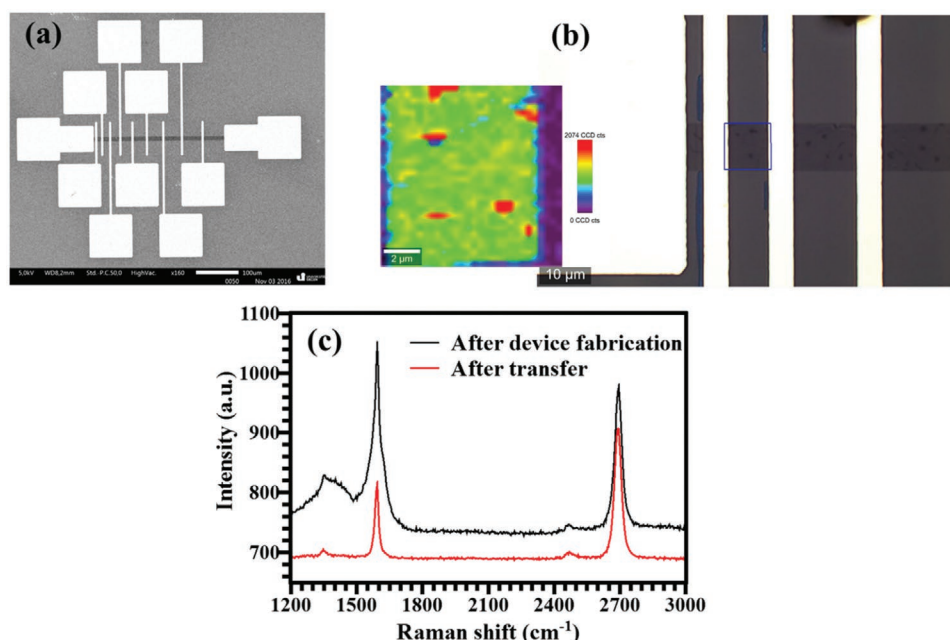


$R_T$ ( $\Omega$ ) - total resistance	$R_{SK}$ ( $\Omega/\square$ ) - sheet resistance of the graphene under metal contact
$d$ ( $\mu\text{m}$ ) - contact length	$\rho_C$ ( $\Omega\text{cm}^2$ ) - specific contact resistivity
$R_C$ ( $\Omega\mu\text{m}$ ) - contact resistance	$R_{CE}$ ( $\Omega$ ) - contact end resistance
$L_{TK}$ ( $\mu\text{m}$ ) - transfer length	$R_{SH}$ ( $\Omega/\square$ ) - sheet resistance of the graphene between the contacts
$W_{CH}$ ( $\mu\text{m}$ ) - channel width	$R_{CF}$ ( $\Omega\mu\text{m}$ ) - contact front resistance
$L_{CH}$ ( $\mu\text{m}$ ) - channel length	

**Figure 1.** a) Measurement setup for TLM structures. b) Equivalent circuit diagram describing the distributed resistive components in a TLM structure. c) Distributed circuit diagram of the transmission line model to describe the G–M contact.  $X = 0$  is the front of the contact and  $X = d$  is the end of the contact ( $d = \text{length of the contact}$ ). The horizontal voltage drop due to the graphene resistance leads to the current crowding at the G–M junction. d) Important notation used in this paper.

graphene after the annealing process. The 2D/G peak intensity ratio was less than 1 with sharper 2D and G peaks. Such features in Raman spectra of annealed graphene samples point toward strong p-doping of substrate-supported graphene in

ambient conditions after the annealing process.<sup>[43–45]</sup> It is worth noticing that the concept of “doping” is used here to describe a change in the Fermi level/carrier density in the graphene due to mirror charges, and not the replacement of graphene atoms

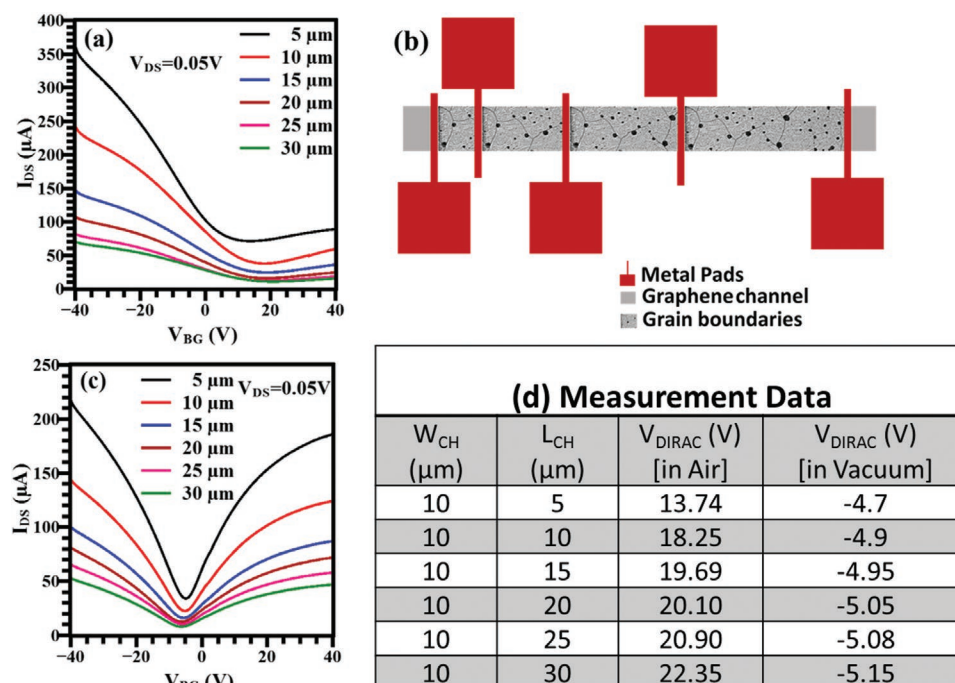


**Figure 2.** a) Scanning electron micrograph of a graphene FET array (TLM structures). b) Raman area map of 2D peak in the area depicted by the blue square in the optical micrograph of the device. c) Raman spectrum of a CVD graphene transferred on a SiO<sub>2</sub>/Si substrate.

by dopants as in conventional semiconductor technology. A broad peak observed near the D peak can be attributed to the amorphous carbon byproducts formed by carbonization of residual polymer layers on graphene surface.<sup>[45]</sup>

Electrical characterization was carried out in a Lakeshore probe station with a Keithley SCS4200 parameter analyzer in

ambient air and in vacuum ( $\approx 10^{-6}$  mbar). The samples were kept in Lakeshore for a period of 48 h to achieve optimum vacuum before measurement. Electrical characterization in ambient atmosphere is carried out by keeping chamber open (humidity  $\approx 21\%$ , temperature  $\approx 300$  K). **Figure 3a** shows the transfer characteristics (source-drain current [ $I_{DS}$ ] vs back-gate voltage [ $V_{BG}$ ])



**Figure 3.** a) Transfer characteristics ( $I_{DS}$ – $V_{BG}$ ) measured in ambient atmosphere (humidity  $\approx 21\%$ , temperature  $\approx 300$  K). b) Schematic diagram of a TLM structure depicting grain boundaries or line defects in the CVD graphene. c) Transfer characteristics ( $I_{DS}$ – $V_{BG}$ ) measured in high vacuum (humidity  $\approx 0\%$ , temperature  $\approx 300$  K, pressure  $\approx 10^{-7}$  mbar). d) Summary of a data in a tabular form focusing on  $V_{DIRAC}$  position measured in ambient air and in vacuum.



of Ni contacted graphene (G–Ni) measured in ambient air. The Dirac voltages are located at positive  $V_{BG}$ , indicating a p-doping of the graphene channel.<sup>[31,32,46]</sup> This is in agreement with Raman measurements (Figure 2c), where signatures of p-doping of graphene were observed. This observation can be ascribed to adsorbed water molecules on top of the graphene surface.<sup>[15]</sup> Graphene acts as an electron donor when water molecules come in contact, leading to the shift of the  $V_{DIRAC}$  toward positive gate voltages, with a charge transfer to graphene per water molecule of  $\approx 0.002e$ .<sup>[47]</sup> We noted a further  $V_{DIRAC}$  shift toward positive  $V_{BG}$  when  $L_{CH}$  increases as summarized in Figure 3d. A similar  $V_{DIRAC}$  shift was observed by Han et al. in a mechanically exfoliated graphene device, and they attributed it to the short channel effects in graphene.<sup>[48]</sup> However, in our case, short channel effects do not apply. Instead, the effect may be attributed to the polycrystalline nature of the CVD monolayer graphene. Grain boundaries in CVD graphene have been shown to act as active sites for adsorbates like water molecules,<sup>[49]</sup> which can be revealed using HF vapor etching.<sup>[50]</sup> In the present case, the number of grain boundaries in a device channel should increase with increasing  $L_{CH}$ , because the device dimensions of the smallest devices are of the same order of magnitude as the grains. Hence, an increased number of grain boundaries in larger devices increase the effect of water adsorbates with  $L_{CH}$ . Figure 3b is the schematic representation of a TLM structure with varied  $L_{CH}$  showing grain boundaries in the CVD graphene.

In vacuum,  $V_{DIRAC}$  is significantly shifted compared to ambient air and is observed near  $-5V$ , that is, the graphene channel is slightly n-doped (Figure 3c). Similar behavior has been observed in Di Bartolomeo et al.<sup>[51]</sup> This indicates successful removal of adsorbates by vacuum. This is confirmed by cycling the devices from ambient conditions to vacuum, which shifts  $V_{DIRAC}$  consistently back and forth between negative and positive voltages (Section A, Supporting Information). We further found that the  $V_{DIRAC}$  difference between different  $L_{CH}$  was negligible under vacuum conditions as reported in Figure 3d. This supports our assumption concerning the significant role played by grain boundaries and other defects as adsorption sites in ambient condition. These results clearly show that vacuum measurements are required for reliable extraction of  $R_{CF}$ . Alternatively, controlled encapsulation with dielectrics may be feasible,<sup>[52]</sup> although this is still a field for further research.<sup>[21]</sup>

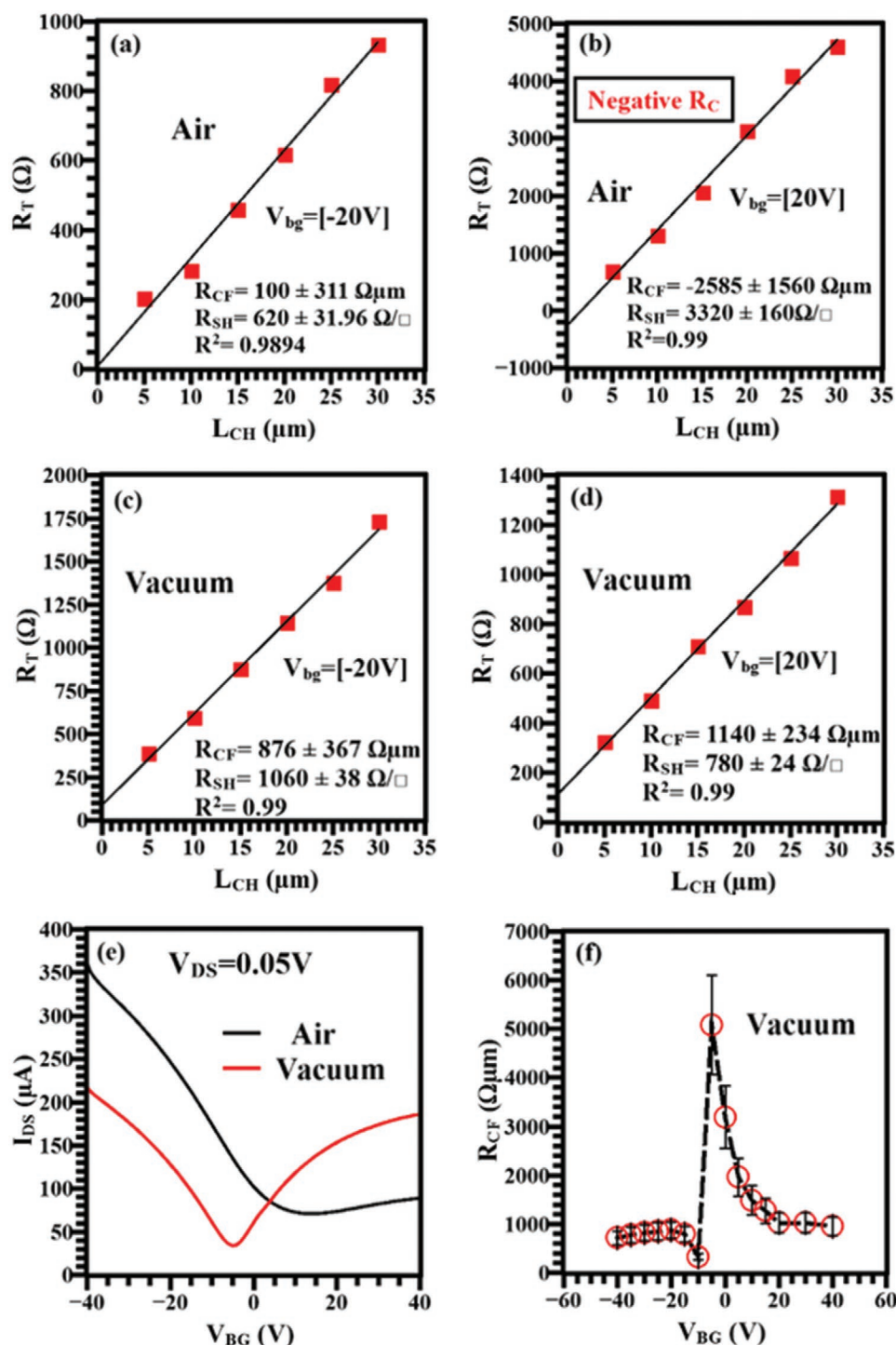
Having established the large impact of the environment conditions on the device characteristics ( $I_{DS}$  vs  $V_{BG}$ ), we now concentrate on the dependable extraction of the parameters related to G–M contacts. The extraction of  $R_{CF}$  for G–Ni contacts (Figure 3a) when the measurement ( $I_{DS}$ – $V_{BG}$ ) were carried out in ambient air results in erroneous values for varying  $V_{BG}$ . For example,  $R_{CF}$  values of  $100 \pm 311 \Omega\mu m$  at  $V_{BG} = -20 V$  (Figure 4a) and of  $-2585 \pm 1560 \Omega\mu m$  at  $V_{BG} = 20 V$  (Figure 4b) are extracted, despite achieving high quality fitting ( $0.97 < R^2 < 0.999$ ) of the  $R_T$  versus  $L_{CH}$  curve. Since negative  $R_{CF}$  values are not possible in any junction, the source for these errors must be in the extraction technique. In contrast, the TLM measurements under vacuum led to reasonable values of  $R_{CF}$ ; in particular  $876 \pm 367 \Omega\mu m$  is extracted at  $V_{BG} = -20 V$  (Figure 4c) and  $1140 \pm 234 \Omega\mu m$  is extracted at  $V_{BG} = 20 V$  (Figure 4d), respectively. This large difference between data in ambient air and high vacuum is also due to

the large distortion induced by the air to the  $I_{DS}$ – $V_{BG}$  curves in Figure 4e ( $L_{CH} = 5 \mu m$  and  $W_{CH} = 20 \mu m$ ). In particular, there is a decrease in the conductivity when the devices are measured in high vacuum, which can be attributed to the removal of water adsorbents from the graphene surface, that provide p-doping to graphene and thus a higher charge density  $n_0$  and a higher conductivity. Figure 4f shows the  $V_{BG}$  dependence of  $R_{CF}$  for the TLM devices measured in high vacuum.  $R_{CF}$  clearly is  $V_{BG}$  dependent, with a peak at  $V_{DIRAC}$ ; while it decreases as the graphene channel is electrostatically doped by  $V_{BG}$ . However, despite measuring the devices in vacuum, the extraction of  $R_{CF}$  leads to an unusually and, more important, unphysically low value at  $V_{BG} = -10 V$ . Current measurements in high vacuum demonstrate a minimum conductance around an approximate  $V_{BG}$  of  $-5V$ ; with this value varying by less than  $0.5 V$  across the TLM array. To avoid this effect of marginal  $V_{DIRAC}$  shifts with varied  $L_{CH}$ , the minimum conductivity points of all the channels were normalized to  $0 V$  to ensure the same  $n_0$  in the graphene channels when comparing the  $R_T$  values as discussed in ref. <sup>[53]</sup> This normalization process was also applied to the measurements done in air, but the obtained results were unphysical (Section D, Supporting Information).

Figure 5a shows the normalized transfer characteristics ( $I_{DS}$  vs  $[V_{BG} - V_{DIRAC}]$ ) for different  $L_{CH}$  of the G–Ni samples measured in vacuum. Figure 5b shows the  $R_{CF}$  values extracted through the TLM method after the normalization. The  $R_{CF}$  values peak at  $(V_{BG} - V_{DIRAC}) = 0$ , where the carrier density in graphene is at its minimum. This suggests that the conventional TLM extrapolation technique for  $R_{CF}$  is valid only when maintaining the same  $n_0$  in graphene channels with different  $L_{CH}$ . A slight difference in the  $n_0$  among the channels leads to large errors in the  $R_{CF}$  values (Figure 4a,b).<sup>[48]</sup>

Figure 5c shows  $R_{CE}$  as a function of  $L_{CH}$  at different  $V_{BG}$  extracted by using the measurement setup shown in Figure 1a.  $R_{CE}$  ranges from  $10.5$  to  $12 \Omega$  with respect to  $L_{CH}$  at a fixed  $V_{BG}$ , demonstrating that  $R_{CE}$  is more or less unaffected by the channel resistance outside the contact.<sup>[33,54]</sup> The  $R_{CE}$  measurement was also carried out in ambient air at  $V_{BG} = 0 V$  (Figure 5d) and was found to be very consistent with the results in vacuum, which indicates that  $R_{CE}$  is unaffected by the channel conductivity and, thus, by the measurements conditions (in this case graphene is protected from water molecules by the contact on the top). Finally,  $R_{CE}$  is rather independent of  $V_{BG}$ . This is most likely because its value is linked to the voltage drop at the end of the contact, where the current density is zero and hence, the  $V_{BG}$  dependence does not manifest.

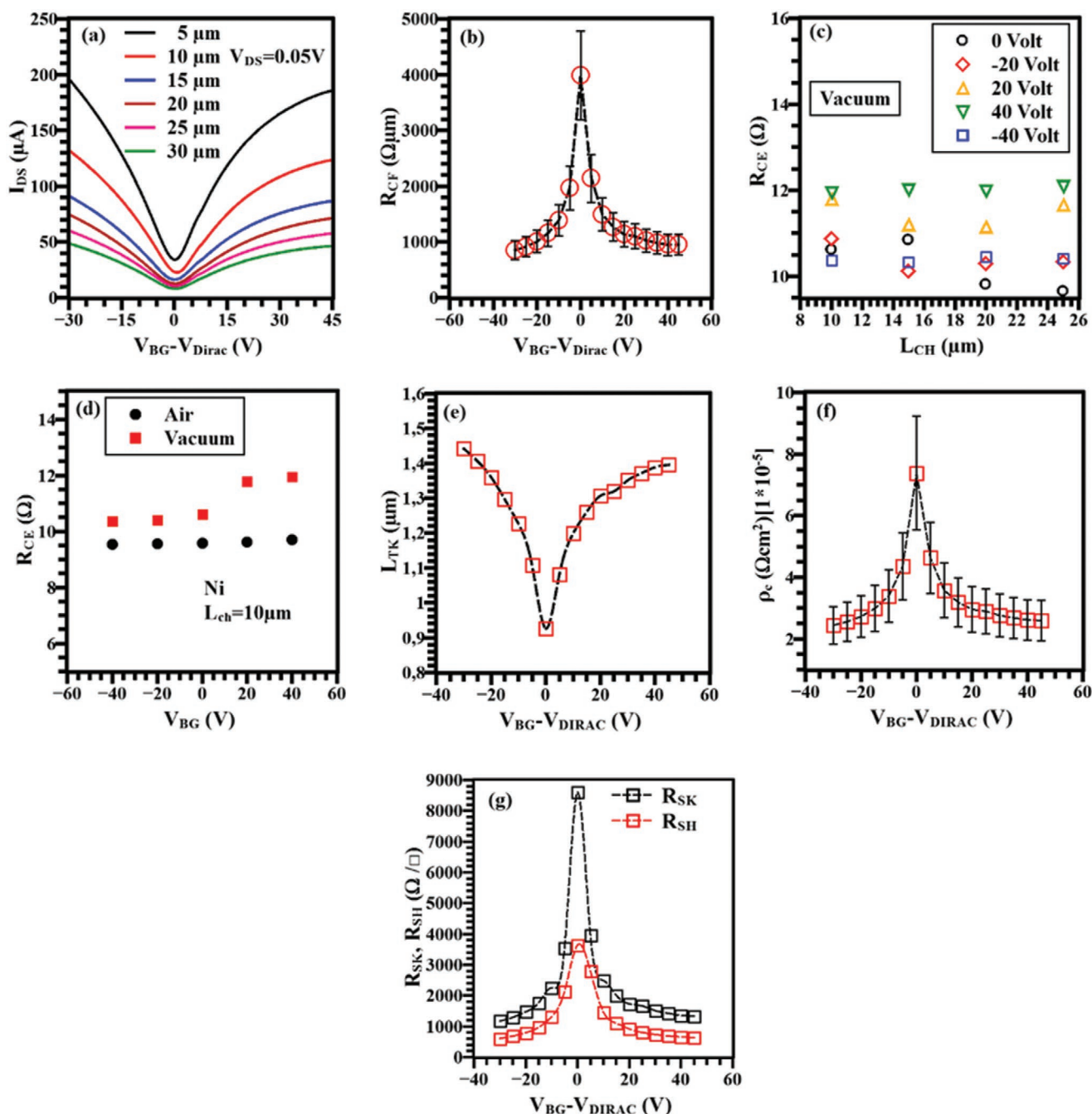
$R_{CE}$  and  $R_{CF}$  values were then used to calculate  $\rho_c$ ,  $I_{TK}$ , and  $R_{SK}$  (Section C, Supporting Information). Figure 5e shows  $I_{TK}$  extracted from measurements done in vacuum as a function of  $(V_{BG} - V_{DIRAC})$ .  $I_{TK}$  is around  $1.4 \mu m$  at  $n_0 = 8.69 \times 10^{12} cm^{-2}$  and decreases to  $0.9 \mu m$  at  $n_0 = 1.01 \times 10^{12} cm^{-2}$ . Figure 5f instead reports the  $\rho_c$  as a function of  $(V_{BG} - V_{DIRAC})$  and  $\rho_c$  is  $2.44 \times 10^{-5} \Omega cm^2$  at  $n_0 = 8.69 \times 10^{12} cm^{-2}$  and  $7.38 \times 10^{-5} \Omega cm^2$  at  $n_0 = 1.01 \times 10^{12} cm^{-2}$ . Error bars indicate upper limits and lower limits in fitting the measured data and they are quite large near  $V_{DIRAC}$ . Finally,  $R_{SH}$  and  $R_{SK}$  were extracted to determine the impact of the metal on the properties of graphene under the contact. Figure 5g shows  $R_{SK}$  and  $R_{SH}$  extracted as a function of  $V_{BG}$ .  $R_{SK}$  for Ni contacts is larger than the  $R_{SH}$ .



**Figure 4.** Extrapolation of  $R_{CF}$  and  $R_{SH}$  by using the transfer characteristics curves of graphene–nickel samples (Figure 3a) measured in ambient atmosphere at gate biases of a)  $-20$  V (p-doped) and b)  $20$  V (n-doped). Red squares represent measured total resistance; black line, is the linear fitting curve.  $R_{CF}$  and  $R_{SH}$  are also extrapolated by using the transfer characteristics curves (Figure 3c) measured in high vacuum at gate biases of c)  $-20$  V and d)  $20$  V. e) Comparison of transfer characteristics measured in air and vacuum. f)  $R_{CF}$  as a function of a  $V_{BG}$ .

Although it has been shown that the p-orbitals of graphene hybridize strongly with Ni d-states,<sup>[55]</sup> the extracted  $\rho_c$  and  $R_{SK}$  are quite high. This can likely be attributed to nickel-carbide formation at the interface, which can be detrimental for the

charge carrier transport through the G–M junction.<sup>[55]</sup> This is even more important at the Dirac point, where  $R_{SK}$  shows a large peak. This is most likely due to the fact that hybridization of graphene orbitals induces small band-gaps at the K-point in



**Figure 5.** a) Transfer characteristics of G–Ni TLM structures after normalizing to  $V_{\text{Dirac}} = 0$  V the curves of Figure 3c. b)  $R_{\text{CF}}$  as a function of a  $V_{\text{BG}} - V_{\text{Dirac}}$ . c)  $R_{\text{CE}}$  as a function of  $L_{\text{CH}}$  measured at different  $V_{\text{BG}}$ . d)  $R_{\text{CE}}$  as a function of  $V_{\text{BG}}$  in ambient atmosphere and in vacuum. e)  $L_{\text{TK}}$  and f)  $\rho_s$  as a function of  $V_{\text{BG}} - V_{\text{Dirac}}$ . g)  $R_{\text{SK}}$  and  $R_{\text{SH}}$  as a function of  $V_{\text{BG}} - V_{\text{Dirac}}$ .

the graphene bands.<sup>[56]</sup> This reduces the graphene charge at the Dirac point, largely impacting the  $R_{\text{SK}}$  value.

As discussed above,  $R_{\text{CF}}$  is intrinsically dependent on the charge density in graphene and in the metal. In the case of metal, it is extremely high and in the order of  $\approx 10^{21} \text{ cm}^{-3}$ , so it does not limit the current and its effect can be neglected. In the case of graphene,  $n_0$  typically varies between  $10^{11}$  and  $10^{13} \text{ cm}^{-2}$ , therefore  $R_{\text{CF}}$  is intrinsically dependent on the  $R_{\text{SK}}$ .<sup>[57]</sup> Therefore, it is important to fabricate high quality graphene to

lower  $R_{\text{SK}}$  and thus to reduce  $R_{\text{CF}}$ .<sup>[58]</sup> Also selecting the metal materials that increase  $n_0$  in the underneath graphene would improve  $R_{\text{SK}}$  and hence  $R_{\text{CF}}$ .

The methodology described for G–Ni contacts was also applied to the case of graphene–copper (G–Cu) and graphene–gold (G–Au) contacts (Section E, Supporting Information). Furthermore, extensive measurements and extractions were also carried out for TLM devices with G–Au contacts measured in ambient air (Section F, Supporting Information). The

**Table 1.** Summary of results.

Graphene–metal contact	$R_{CF}$ [ $\Omega\mu\text{m}$ ]	$L_{TK}$ [ $\mu\text{m}$ ]	$R_{SK}$ [ $\Omega\text{ }\square^{-1}$ ]	$R_{SH}$ [ $\Omega\text{ }\square^{-1}$ ]	$\rho_c$ [ $\Omega\text{cm}^2$ ]
G–Ni ( $n = 8.69 \times 10^{12} \text{ cm}^{-2}$ )	$853 \pm 171$	1.45	1174	608	$2.44 \times 10^{-5}$
G–Cu ( $n = 1.15 \times 10^{13} \text{ cm}^{-2}$ )	$860 \pm 172$	1.63	417	729	$1.1 \times 10^{-5}$
G–Au ( $n = 1.07 \times 10^{13} \text{ cm}^{-2}$ )	$395 \pm 79$	1.68	376	425	$7.16 \times 10^{-6}$
G–Ni ( $n = 1.01 \times 10^{12} \text{ cm}^{-2}$ )	$3984 \pm 799$	0.93	8599	3642	$7.38 \times 10^{-5}$
G–Cu ( $n = 1.34 \times 10^{12} \text{ cm}^{-2}$ )	$3664 \pm 733$	0.97	3359	3540	$3.5 \times 10^{-5}$
G–Au ( $n = 1.06 \times 10^{12} \text{ cm}^{-2}$ )	$1303 \pm 261$	0.97	1081	2700	$1.56 \times 10^{-5}$

measurements in ambient air and vacuum confirm the previous findings, with a large positive  $V_{\text{DIRAC}}$  under ambient air and smaller  $V_{\text{DIRAC}}$  values under vacuum (with similar values of  $\approx 0.7 \text{ V}$  for the different  $L_{\text{CH}}$ ). The details of these measurements are reported in Section E, Supporting Information. The complete set of experimental results is summarized in Table 1.

## 4. Conclusions

The effects of measurement conditions on the extraction of contact related parameters in G–M junctions were investigated in detail using back-gated TLM structures for different metals. Measurements carried out in ambient conditions, irrespective of the used contact metal, resulted in highly asymmetric transfer curves with positive  $V_{\text{DIRAC}}$  values, indicating strong p-doping of the graphene channel. Also, a  $V_{\text{DIRAC}}$  shift in devices with different  $L_{\text{CH}}$  was observed which is explained on the basis of polycrystalline nature of CVD graphene with non-uniform grain boundary density.

Vacuum measurements, in contrast, yielded highly symmetric transfer curves for each used metal, which can be reliably used to extract the G–M junction parameters, eliminating one of the main reasons for the scattered values of  $R_{\text{CF}}$  (and  $\rho_c$ ) reported in the literature.

Discrepancies related to the extraction of  $R_{\text{CF}}$  (and  $\rho_c$ ) via the TLM method were also discussed rigorously. In particular, to extract dependable  $R_{\text{CF}}$  values, the  $n_0$  in the graphene between the contacts should be kept constant for the different devices ( $L_{\text{CH}}$ ), and hence small differences in  $V_{\text{DIRAC}}$  position should be compensated.  $R_{\text{CF}}$  is strongly dependent on the  $n_0$  in the graphene underneath the metal, with the lowest value achieved for gold contacts. The present study highlights the importance of a careful extraction of the contact related parameter in G–M junctions.

## Supporting Information

Supporting Information is available from the Wiley Online Library or from the author.

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## Conflict of Interest

The authors declare no conflict of interest.

## Keywords

contact resistances, chemical vapor deposited graphenes, graphene–metal contacts, sheet resistances, specific contact resistivities, transfer length methods, transmission line models

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